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1	Single step electrodeposition of superhydrophobic black NiO thin films
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9	Highlights
10 11 12 13	<ul> <li>Electrodeposition of superhydrophobic black NiO films on Cu is studied.</li> <li>Superhydrophobicity is attributed to the formation of a rough surface.</li> <li>An improvement of the corrosion resistance of Cu sub-layers is observed.</li> </ul>
14	Abstract
15 16 17 18	Black finished surfaces have extensive applications in many domains, such as optics, solar cells, and aerospace. The single step electrodeposition of superhydrophobic black NiO films from a dimethyl sulfoxide based electrolyte is described in this paper. The physicochemical properties of the obtained film were characterized using Scanning Electron Microscopy, X-ray Diffraction,

and electrochemical tests (Electrochemical Impedance Spectroscopy and potentiodynamicpolarization). A rough surface with a low reflection of light was formed after the deposition

21 process that increased the contact angle of water from about 87° (for bare Cu) to 163° (in 22 presence of the black coating), which improved the corrosion resistance of the Cu substrate by

about 30%. The formed black NiO film revealed a notably high stability and kept its appearance

even after corrosion tests.

25 Keywords: Black NiO, Superhydrophobic, Corrosion, Electrodeposition, thin films

26

# 27 **1. Introduction**

Black finished surfaces are useful for optical instruments, solar cells, black 28 decorative coatings, and for defense and aerospace industries [1,2]. There are 29 several studies regarding black finished surfaces, including black Si, black Cr, and 30 black Ni [2-4]. Black Ni surfaces are normally obtained by etching a low P content 31 Ni-P (1-4 wt.% P) in an oxidizing acid [5,6]. Etching forms several cracks on the 32 surface of the Ni-P film. These cracks, providing multiple reflection and absorption 33 sites for incident light, are responsible for the black aspect of the surface [7]. 34 However, the film also becomes very vulnerable to corrosion due to these cracks 35

[1]. Furthermore, blackening the surface by chemical etching induces a hugematerial loss that is not economical [8].

The corrosion of metals can be effectively blocked by decreasing the contact of the 3 surface with the corrosive media. Superhydrophobic materials, i.e. surfaces with a 4 water contact angle larger than 150° [9], reduce the corrosion, because the contact 5 between the oxidizing media and the surface of the sample is reduced. Therefore, 6 superhydrophobic films are known to offer an outstanding corrosion resistance 7 [10–12]. Superhydrophobic films also offer self-cleaning, anti-fouling, and frost 8 prevention properties. Superhydrophobicity can be obtained by modification of a 9 surface owing to the surface energy decrease and the formation of a rough 10 hierarchical surface morphology [13]. 11

NiO is formed by oxidation at the surface of Ni-P during chemical etching. NiO is 12 a p-type semi-conducting oxide with a fcc crystalline structure exhibiting a good 13 chemical stability [14,15]. Several methods including annealing [17], sol-gel 14 chemistry [18], ionic layer adsorption and reaction (SILAR) [19], and 15 electrodeposition [20] have been investigated to form NiO. Electrodeposition has 16 various advantages such as the ability to coat large surfaces, a homogenous 17 deposition, a controllable morphology and thickness, high adhesion to the 18 substrate, and few problems related to inter-diffusion [20]. Koussi et al. [20] have 19 successfully electrodeposited NiO from a dimethyl sulfoxide (DMSO) based 20 21 electrolyte. The mechanism of the electrodeposition of NiO in DMSO was described by the following equations in the absence (1) and in the presence of a 22 low content of water (2), respectively: 23

$$25 \quad Ni^{2+} + O^{2-} \to NiO \tag{1}$$

24

 $Ni^{2+} + 20H^- \rightarrow Ni(0H)_2 \rightleftharpoons Ni0 + H_20$  (2)

27

In this paper, we report for the first time the single-step electrodeposition of a black superhydrophobic NiO coating from a DMSO-based electrolyte. The coating was characterized using Scanning Electron Microscopy (SEM), grazing incidence X-Ray Diffraction (grazing XRD), Water Contact Angle measurements (WCA), Electrochemical Impedance Spectroscopy (EIS) and potentiodynamic polarization tests.

34

#### **2. Experimental procedure**

The electrodeposition electrolyte was a DMSO based solution at 50°C, containing 2  $190 \text{ g.L}^{-1} \text{ NiSO}_4$ .  $6\text{H}_2\text{O}$ ,  $10 \text{ g.L}^{-1} \text{ NiCl}_2$ .  $6\text{H}_2\text{O}$ ,  $8 \text{ g.L}^{-1} \text{ H}_3\text{PO}_3$ ,  $16 \text{ g.L}^{-1} \text{ H}_3\text{BO}_3$ , and 3  $5 \text{ mL.L}^{-1} \text{ H}_3\text{PO}_4$ . All the chemicals, provided by Sigma-Aldrich, were highly pure 4 and used as received.

Cyclic voltammetry and potentiostatic electrodeposition experiments were 5 performed with a potentiostat/galvanostat (VersaSTAT 3). Before the deposition, 6 the Cu substrate was pre-treated according to reference [21]. A common 3-7 electrode setup was used consisting of the Cu substrate as working electrode, a Pt 8 plate as counter electrode, and an Ag/AgCl (KCl saturated) as reference electrode. 9 For cyclic voltammetry tests, the potential was gradually decreased from 0 V vs. 10 the reference electrode, to -1.5 V and then increased to 0 V. The scan rate was 20 11 mV.s<sup>-1</sup>. The electrodeposition was achieved by chronoamperometry. A constant 12 potential of - 1V vs. the reference electrode was applied on the working electrode 13 for 1200 s, while the solution was stirred with a speed of 650 rpm. 14

Two scanning electron microscopes (Philips XL 30 ESEM, and CARL
ZEISS/Ultra 55) were used to study the surface and cross-section morphologies,
respectively. The chemical composition of the films was investigated by Energy
Dispersive Spectroscopy (EDS).

The sample reflectance was recorded using an UV-visible spectrophotometer (Varian Cary 300) equipped with an integrating sphere DRA-CA-30I in the 380-800 nm range. Measurements were performed 4 times for each sample by rotating the sample holder in order to probe the whole surface of the samples.

A Siemens D5000 diffractometer was employed to investigate the crystalline structure. XRD patterns were obtained over the 2 $\theta$  range of 30–60° (with 0.04° step size) using Cu K $\alpha$  radiation ( $\lambda = 0.15406$  nm) generated at 30 mA and 40 kV.

A tensiometer (Adimec MX12P) was used to do the water contact angle
measurements (2 μL droplets) at five different locations. Drop analysis LB-ADSA
plugin in ImageJ software was used to measure the contact angle [22].

The corrosion resistance of the films was studied after 60 minutes immersion in a 30 3% NaCl solution by EIS and Tafel tests. The EIS measurements were done at 31 Open Circuit Potential (OCP) in a frequency range from 100 kHz to 10 mHz with 32 10 mV peak-to-peak voltage amplitude. Zview was used to analyze the obtained 33 EIS data. Potentiodynamic polarization experiments were carried out at a scan rate of 0.5 mV/s from -300 mV (vs. OCP) to 500 mV (vs. reference electrode). The
results were normalized by the exposed area to the corrosive media.

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## 3. Results and Discussion

## • Cathodic electrodeposition

The cyclic voltammetry curves of the cathodic electrodeposition of Ni from the 6 DMSO based electrolyte are presented in Figure 1. It can be seen that the current 7 density at -1 V is relatively low. Such a low value makes it kinetically favorable 8 for the nucleation and growth to occur at preferential sites. Such type of 3D 9 "island" growth (described by the Volmer-Weber model) is known to form a rough 10 deposit. Figure 2 depicts the current density during the deposition of the film in 11 DMSO at -1 V. The current density for NiO deposition from DMSO is notably 12 lower than previously reported for Ni deposition from an aqueous electrolyte [21]. 13 This observation points to the higher resistivity and lower throwing power in 14 DMSO than in aqueous electrolytes, leading to a reduced deposition rate. 15

• Surface and cross-section morphology

Figure 3 shows the surface and cross-section morphologies of the black coating. In 17 Figure 3A, the black appearance of the coating is obvious. The SEM image 18 presents a surface made of several hierarchical island shape features that are 19 regularly distributed over the surface. Such a morphology (that is similar to the 20 known lotus leave morphology [23]) highly decreases the light reflection (Figure 21 4) and thus makes the surface look black. The increase in the reflection of the Cu 22 substrate at around 550 nm is due to the natural color of Cu. Moreover, such a 23 morphology offers a high roughness that increases the water contact angle (see 24 below). The cross-section shows several well-distributed nanometric island shape 25 features on the surface. Moreover, the formed black film was notably adhesive, 26 since no cracks or delamination was observed at the interface between Cu and the 27 coating. 28

• Chemical composition and structure

The chemical composition of the film is summarized in Table 1. A film composed of a mixture of NiO and Ni-P is formed on pure Cu. The high Cu content is due to the low thickness of the black film. The presence of S and C in the chemical composition is due to the incorporation of DMSO inside the film [20].

Figure 5 shows the grazing incidence XRD pattern of the black film. The strong sharp peak at 43.5 ° is attributed to the NiO (200) reflection (NiO presents a NaCltype structure) [14,16] that shows the preferential growth of the film. The absence of Ni peaks can be attributed to the amorphous nature of the Ni-P film. The average grain size D was estimated to be around 100 nm using the Debye Scherrer formula [14],

$$7 \quad D = \frac{0.9\lambda}{\beta \cos\theta} \tag{3}$$

8 where  $\lambda$  is the X-ray wavelength,  $\beta$  is the full width at half maximum of the peak, 9 and  $\theta$  is the diffraction angle. The grain size of the black film is notably bigger 10 than that previously reported elsewhere [14,16,24]. The formation of bigger grains 11 might be related to the low deposition rate from DMSO.

• Water contact angle

The water contact angle of the Cu substrate and the black film are shown in Figure 6. The contact angle values for the Cu substrate and the film were  $83 \pm 6^{\circ}$  and 161  $\pm 3^{\circ}$ , respectively. Therefore, applying the black NiO film changed the hydrophilic Cu surface to a superhydrophobic surface.

The hydrophobicity of these films was previously found to be due to the roughness of the surface [25]. The superhydrophobicity of the surface comes from the heterogeneous wetting, which means that the trapped air prevents the liquid from penetration [26]. This can be expressed by the following equation:

21 
$$\cos \theta^* = f(1 + \cos \theta) - 1$$
 (4)

<sup>22</sup> Where f is the area fraction of the droplet in contact with the solid (and thus 1-f is <sup>23</sup> the area fraction of the droplet in contact with the trapped air), and  $\theta^*$  and  $\theta$  are the <sup>24</sup> contact angles of the rough coating and the substrate (or flat surface). The f value <sup>25</sup> calculated for the black NiO film is 0.049: it has a very low wetting ability, notably <sup>26</sup> lower than some previously reported values for superhydrophobic Ni films (0.25 <sup>27</sup> [27], and 0.13 [28]).

• Corrosion resistance

A typical impedance spectrum of the black NiO film is depicted in Figure 7. The film presents one time constant in its EIS data. The Randles model, which is the typical model to fit the EIS data of electrodeposited superhydrophobic NiO films [12,25,29], was employed to analyze the black NiO film. A Constant Phase Element (CPE) was used to describe the non-ideal behavior of the interface. The
 impedance of a CPE is defined as:

$$3 \quad Z_{CPE} = \frac{1}{Y_0(i\omega)^n} \tag{5}$$

 $Y_0$  is the constant of admittance, *i* is the imaginary unit,  $\omega$  is the angular frequency, 4 and n is the CPE exponent [30]. n is also sometimes considered as the roughness 5 factor since it is affected by the surface roughness [31]. The analyzed data of the 6 black NiO film and Cu substrate (that is reported in [21]) are presented in Table 2. 7 Note that the Cu substrate had an extra Warburg element in its equivalent circuit 8 that expressed the diffusion-limitation of corrosion. The value of n for the Cu 9 substrate and the black NiO film were 0.80 and 0.76, respectively. The n value for 10 the substrate is low due to the presence a Warburg element. This observation is 11 pointing out that the black NiO has a rougher surface. The modulus Y° is higher 12 than the value expected for a "metallic" electrode. Rough surfaces have a higher 13 specific capacitance than flat ones, and increasing the roughness of thin films will 14 enhance their capacitance [32]. Moreover, electrodeposited NiO has been shown to 15 have a high pseudocapacitance, useful for supercapacitor applications [33-35], 16 attributed to some contribution of chemical capacitances. 17

Applying the thin black NiO film increased the corrosion resistance by about 25% (8.1 vs. 6.1 k $\Omega$ .cm<sup>2</sup> for NiO and Cu, respectively).

Figure 8 shows the polarization curves performed on the black NiO film and the bare Cu substrate. The Tafel extrapolation method was used in a potential range of  $\pm 250$  mV around OCP, to obtain the corrosion potential (E<sub>corr</sub>), corrosion current density (i<sub>corr</sub>), and anodic and cathodic slopes ( $\beta_a$  and  $\beta_c$ ). The Stern-Geary equation was used to calculate the polarization resistance [36]. Table 3 summarizes these data for the black NiO film.

$$26 \quad R_P = \frac{\beta_a \beta_c}{2.303(\beta_a + \beta_c)i_{corr}} \tag{6}$$

In comparison with the reported data for the Cu substrate [21], the black NiO film notably shifted the corrosion potential (+155 mV) to more anodic regions. This means a significant decrease in corrosion inclination [37]. The polarization resistance (6.4 and 9.5 k $\Omega$  for Cu and black NiO, respectively) shows about 33% increase, in good agreement with EIS results. The black NiO coating presents especially a lower current density at high potentials showing its high chemical stability.

Figure 9 shows that the surface morphology of the black NiO after the corrosion 1 tests is clearly unchanged. The chemical composition of the surface after the 2 corrosion tests is presented in Table 1. A comparison of the chemical composition 3 of the black NiO film before and after the corrosion tests reveals that the amount of 4 O increased, while the content of Ni decreased. A part of the Ni of Ni-P was 5 dissolved, so the surface was enriched with other components (i.e. O and S), in 6 agreement with the common corrosion mechanism of Ni films [37]. Therefore, the 7 superhydrophobicity of the electrodeposited black NiO film strengthens the 8 chemical stability and substantially improves the corrosion resistance. 9

10

## 11 **4.** Conclusions

The single step electrodeposition of superhydrophobic black NiO coatings from a DMSO based electrolyte is presented in this paper. A very rough surface containing many well-distributed island shaped features is formed that decreases the light reflection and increases the water contact angle.

The corrosion resistance increases by about 30% due to the superhydrophobicity of the surface that limits the contact between the surface and corrosive media. The effect of the deposition parameters on the properties of the black NiO film and the possibility to form it on other substrates, such as Al or Ti, is interesting for aerospace applications and will be the subject of a future study.

21

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- 26

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- 4 25-30. doi:10.1016/j.surfcoat.2013.01.053.

- 2 Tables

#### 4 Table 1. Chemical composition of the black coating before and after corrosion tests

Element	Before corrosion tests: Wt.%	After corrosion tests: Wt.%		
С	3.6	3.2		
0	11.0	13.9		
Р	2.6	2.8		
S	7.8	8.8		
Ni	61.8	56.2		
Cu	13.2	15.1		

#### 7 Table 2. EIS fit values of the black NiO film and Cu substrate

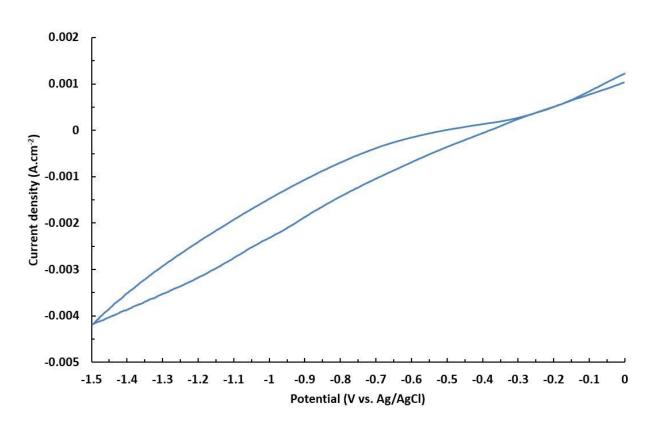
Sampla	R <sub>s</sub> (Ω.cm <sup>2</sup> )	CPE <sub>dl</sub>		R <sub>ct</sub>	W		
Sample		$\begin{array}{c} Q\\ (\mu F.cm^{-2}.s^{n-1}) \end{array}$	n	$(k\Omega.cm^2)$	W-R (k $\Omega$ .cm <sup>2</sup> )	W-T s	W-P
Black NiO	7.5	578.2	0.76	8.1	-	-	-
Cu Sub. [21]	20.3	129.8	0.80	0.02	6.1	165.9	0.43

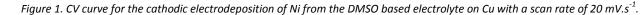
Table 3. Corrosion current density, corrosion potential, anodic and cathodic slopes, and polarization resistance of the black NiO
 film

Sampla	i <sub>corr</sub> (µA.cm <sup>-2</sup> )	E <sub>corr</sub> (mV) vs. Ag/AgCl	Average Tafel slope (mV. dec <sup>-1</sup> )		R <sub>p</sub>	
Sample			$\beta_a$	$\beta_c$	$(k\Omega.cm^2)$	
Black NiO	1.64	-45	44	149	9.5	
Cu Sub. [21]	3.32	-200	66	195	6.4	

#### **Figures**







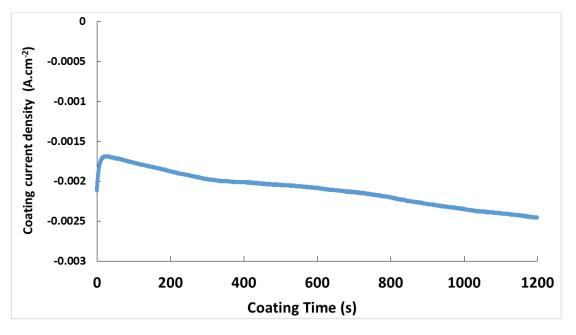
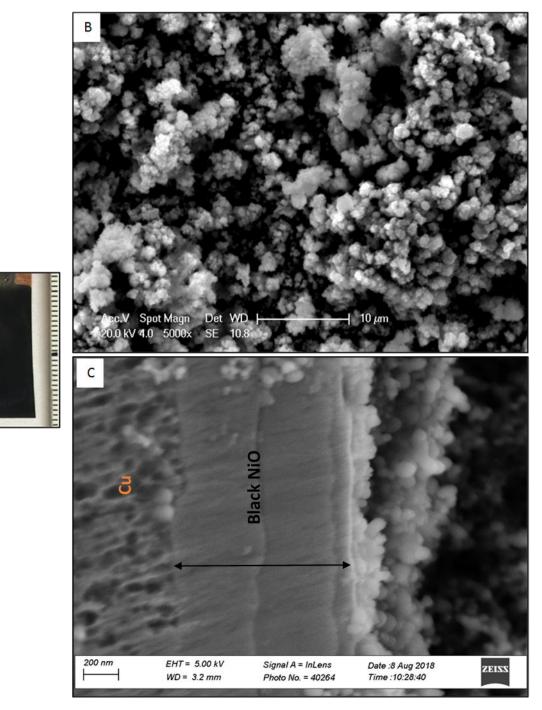


Figure 2. Current density as a function of the coating time for a black NiO film obtained in DMSO.





A

Figure 3. (A) Black NiO film on Cu and its surface (B) and cross-section (C) morphology.

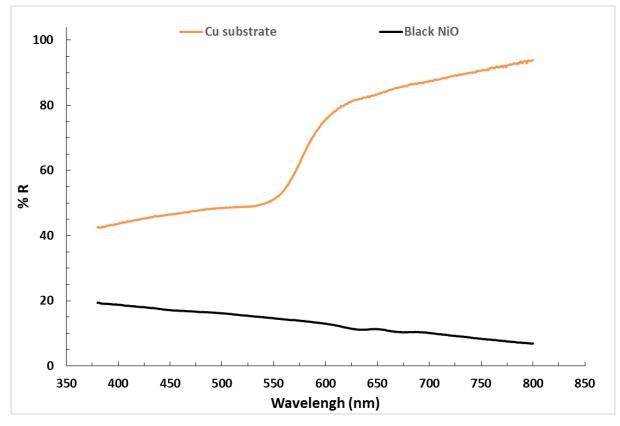
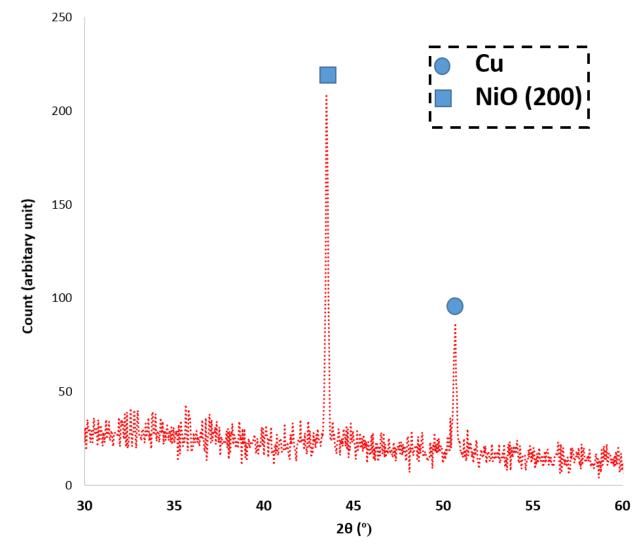
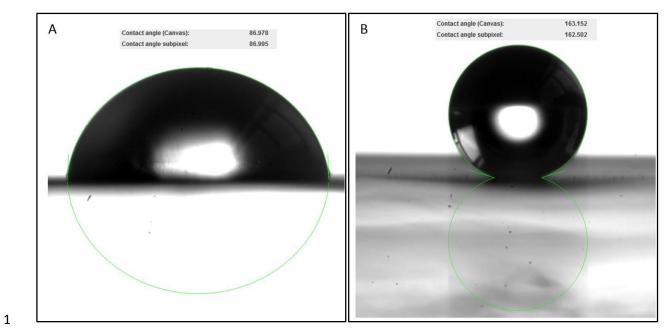


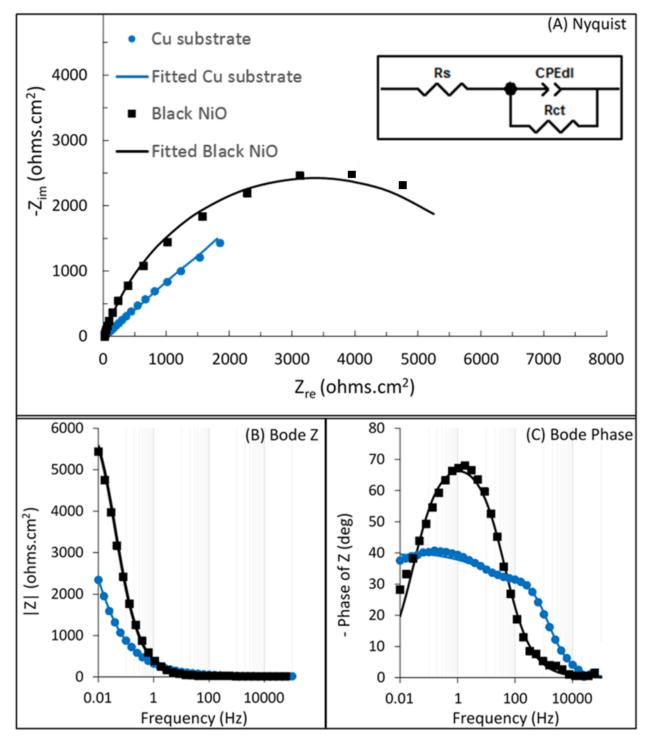
Figure 4. Reflectance of Cu substrate and black NiO film as a function of the wavelength of light.

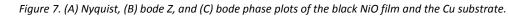


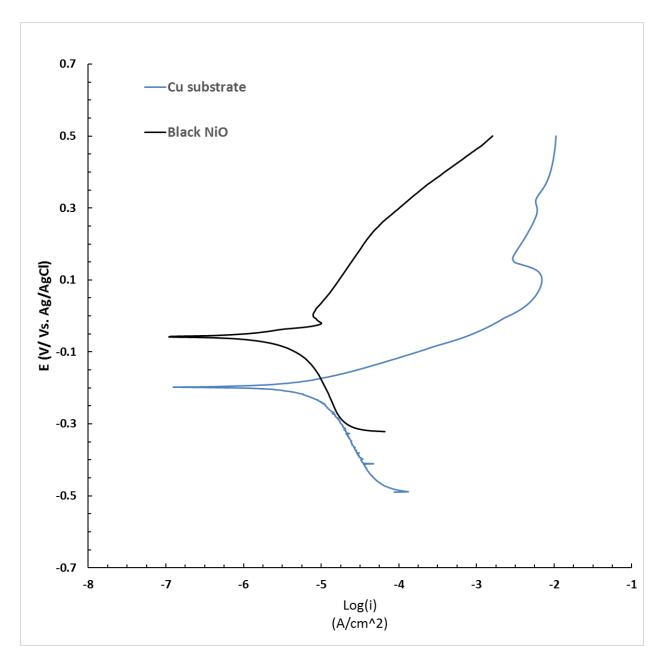
2 Figure 5. Grazing incidence XRD pattern of the black NiO coating.



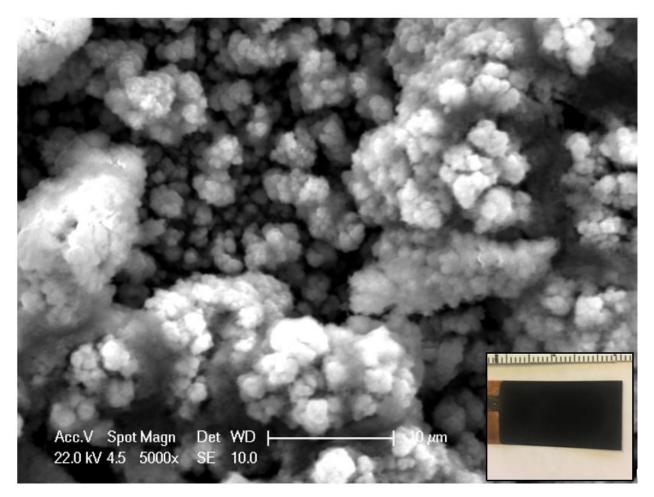
2 Figure 6. Contact angle between a 2µL water droplet and (A) the Cu substrate, (B) the black NiO film.







2 Figure 8. Tafel plots of the black NiO film and the Cu substrate.



2 Figure 9. The general aspect and surface morphology of the black NiO film after the corrosion tests.